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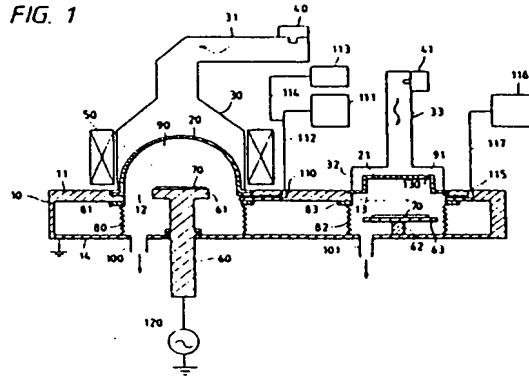
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## 54 Sample treating method and apparatus.

(57) A sample treating method and apparatus for treating a sample such as a semiconductor element substrate or the like, by etching and anticorrosion-treatment, uses an anticorrosion gas plasma to remove adhered matters formed by the etching of the sample. The anticorrosion gas comprises halogen gas or inert gas. Wet-type anticorrosion treatment is not required, enabling the throughput to be improved in treating the samples. Both etching and anticorrosion treatment may take place in the same chamber (90). Passivation treatment, e.g. by oxygen plasma or ozone, may take place subsequently in a separate chamber (91).

FIG. 1



SAMPLE TREATING METHOD AND APPARATUS

The present invention relates to a sample treating method and an apparatus, and more particularly to a method and an apparatus for treating samples such as semiconductor element substrates that are to be etched as well as to be anticorrosion-treated.

In etching samples such as semiconductor element substrates having, for example, an aluminum film, an aluminum alloy film, or a multi-film structure consisting of these films and a barrier metal using the plasma of a halogen gas, a problem arises in regard to corrosion when they are exposed to the atmosphere after etching. Therefore, these samples must be anti-corrosion-treated in addition to being etched. In order to cope with such requirements, there have heretofore been proposed the following technologies.

Japanese Patent Publication No. 30268-1987 discloses a technology of dry-etching and after-treatment according to which an aluminum film or an aluminum alloy film such as of aluminum-silicon, aluminum-copper, or aluminum-silicon-copper is dry-etched in a vessel using a halogen compound gas which is active, followed by the treatment with the plasma of a mixture gas consisting of fluorocarbon and oxygen without taking it out of the vessel.

Further, Japanese Patent Publication No. 12343-1983 discloses a technology which exposes the etched aluminum film or the aluminum alloy film to the fluorination plasma in order to prevent the film etched by using the chlorination plasma from corroding after etching.

According to such technologies, however, it is difficult to remove corrosive matters that are formed during the etching of the samples and that adhere to the side walls of the patterns. In such prior technologies, furthermore, the substitution reaction (substitution into  $\text{Al}_2\text{O}_3$  due to the reaction of, for example,  $\text{AlCl}_3$ , which is a component of the corrosive matter that adheres with, for example, oxygen which is a component of gas plasma in the after-treatment) takes place on the surface layer only of the corrosive matter that adheres to the side walls of the pattern, and does not proceed into the corrosive matter that adheres. When the samples are exposed to the atmosphere, furthermore, water content in the open air infiltrates into the corrosive adhered matter which is not dense, whereby the reaction takes place between the infiltrated water content and the corrosive adhered matter to form a corrosive component (e.g., hydrochloric acid) that corrodes the samples. According to the conventional technologies, as described above, the samples after etching do not have sufficient resistance against the corrosion. In dealing with modern multi-layer films consisting of aluminum and other materials or aluminum alloy films containing copper, in particular, corrosion develops due to the so-called cell action (aluminum works as an anode), the degree of corrosion is accelerated, and lack of resistance against the corrosion becomes more conspicuous.

Therefore, these samples have generally been anticorrosion-treated by the wet system after etching as disclosed in, for example, Japanese Patent Laid-Open No. 133388-1986. The wet-type anticorrosion treatment makes it possible to remove corrosive matters adhered to the side walls of the pattern of the samples and to increase resistance of the samples against the corrosion in the open air after etching.

According to the above prior art processes which anticorrosion-treat the samples based on the wet system after etching, any water content remaining after the wet-type anticorrosion treatment reacts with a component containing, for example, chlorine that remains after the wet-type anticorrosion treatment or reacts with chlorine in the open air to form hydrochloric acid ( $\text{HCl}$ ) which is a corrosive component. Therefore, the samples are corroded after the wet-type anticorrosion treatment. Inevitably, therefore, the drying is required after the wet anticorrosion treatment.

Therefore, the known processes involve the following problems.

(1) An extended period of time (at least wet-type anticorrosion treatment time plus dry treatment time) is required before the anticorrosion treatment of samples is finished after etching, and the throughput decreases.

(2) The cost of the apparatus increases and an increased area is occupied by the apparatus when the samples after etching are anticorrosion-treated using a wet-type anticorrosion treatment apparatus and another dry-treatment apparatus (needing means for conveying the samples between these apparatuses as a matter of course).

(3) Apparatuses are needed to recover waste liquor from the wet-type anticorrosion treatment and to treat the waste liquor, causing the apparatus to become complex and pushing up the cost.

The object of the present invention is to provide a sample treating method which effects the etching and maintaining an increased throughput in treating the samples that require anticorrosion treatment, and to provide an apparatus therefor.

The invention provides a sample treating method comprising at least a step for anti-corrosion-treating

an etched sample by utilizing a plasma of a gas containing a halogen gas or an inert gas as an anticorrosion gas that is capable of removing from said etched sample adhered matters containing halogen formed by the etching of said sample. The invention also provides a sample treating apparatus comprising means for plasmatizing a gas containing a halogen gas or inert gas as an anticorrosion gas that is capable of removing adhered matters containing halogen formed by the etching of said sample, means for holding said etched sample that is anticorrosion-treated by utilizing the plasma of said anticorrosion gas, and a treating chamber that is evacuated and contains said sample-holding means therein.

Fig. 1 is a diagram illustrating the constitution of a plasma-etching apparatus according to an embodiment of the present invention;

Fig. 2 is a vertical section view illustrating principal portions of a sample treated by the plasma-etching apparatus of Fig. 1; and

Fig. 3 is a vertical section view illustrating principal portions of the sample of Fig. 2 after etching.

The interior of the treating chamber is evacuated by evacuation means. The samples are held by sample holding means in the treating chamber. An etching gas is introduced into the treating chamber by gas introducing means. An etching gas in the treating chamber is plasmatized by plasmatizing means. The sample held by sample holding means is etched with the plasma. An anticorrosion gas is also introduced into the treating chamber by gas introducing means. The anticorrosion gas in the treating chamber is plasmatized by plasmatizing means. The sample held by sample holding means is treated by utilizing the plasma.

The antcorrosion treatment of the samples that is carried out by utilizing the plasma of the anticorrosion gas easily removes reaction products that are formed by the etching of the samples and that adhere to the samples as well as etching gas components that are corrosive in the open air (hereinafter referred to as adhered matters), without forming any new adhered matter.

Therefore, no wet-type anticorrosion treatment is necessary making it possible to greatly reduce the time required before the anticorrosion treatment of the sample is finished.

An embodiment of the present invention will now be described in conjunction with Figs. 1 to 5.

In Fig. 1, two openings 12 and 13 are formed maintaining a predetermined distance and a diameter in a top wall of a buffer chamber 10. Means (not shown) for evacuating the interior of the buffer chamber 10 is provided in the buffer chamber 10. A discharge tube 20 is air-tightly provided on the top wall 11 of the buffer chamber 10 corresponded to the opening 12. The discharge tube 20 in this case has nearly a hemispherical shape. A waveguide 30 is arranged on the outside of the discharge tube 20 so as to include the discharge tube 20 therein. The axis of the waveguide 30 is in agreement with that of the discharge tube 20. The waveguide 30 and a magnetron 40 that is means for generating microwaves are coupled together via another waveguide 31. Magnetic field generating means such as a solenoid coil 50 surrounds the waveguide 30 being nearly corresponded to the discharge tube 20. The solenoid coil 50 is electrically connected to a power source (not shown) via current adjusting means (not shown). A sample table shaft 60 has its upper portion protruded into the buffer chamber 10 and into the discharge tube 20 and has its lower portion protruded beyond the buffer chamber 10 so as to be airtightly inserted in a bottom wall 14 of the buffer chamber 10. A sample table 61 is provided nearly horizontally at the upper end of the sample table shaft 60. The sample table 61 has the shape of a plane which is smaller than the opening 12 but is greater than a sample 70. The sample table 61 has a plane for placing the sample on the front surface thereof, i.e., on the surface corresponded to the top of the discharge tube 20. The axes of the sample table shaft 60 and of the sample table 61 are nearly in agreement with the axis of the discharge tube 20. A metallic bellows 80 is provided in the buffer chamber 10 to surround the sample table shaft 60. The lower end of the bellows 80 is provided inside the bottom wall 14 of the buffer chamber 10. A flange 81 is attached to the upper end of the bellows 80. A sealing ring (not shown) is provided on the surface of the flange 81 that is opposed to the inner surface of the top wall 11 of the buffer chamber 10. Means (not shown) is also provided to expand and contract the bellows 80. Space 90 is defined being airtightly shut off from the interior of the buffer chamber 10 under the condition where the bellows 80 is expected by expansion-contraction drive means and the flange 81 is pressed via the sealing ring onto the inner surface of top wall 11 of the buffer chamber 10. An evacuation nozzle 100 is formed in the bottom wall 14 of the buffer chamber 10 to be communicated with the space 90. An evacuation pipe (not shown) coupled to an evacuation device (not shown) is coupled to the evacuation nozzle 100. The evacuation pipe is provided with a switching valve and an evacuation resistance variable valve (not shown). A gas introduction path 110 is formed in the top wall 11 of the buffer chamber 10 so as to be communicated with the space 90. A gas introduction pipe 112 coupled to a source 111 of etching gas is connected to the gas introduction path 110. The gas introduction pipe 112 is provided with the switching valve and a gas flow rate control device (not shown). Further, a gas introduction pipe 114 coupled to a source 113 of anticorrosion gas is coupled to the gas introduction pipe 112 on the downstream

side of the switching valve and the gas flow rate control device that are provided for the gas introduction pipe 112. The gas introduction pipe 114 is provided with the switching valve and the gas flow rate control device (not shown). The gas introduction pipe 114 may be directly coupled to the gas introduction path 110. There is provided a power source for applying a bias such as a high-frequency power source 120. The sample table 61 is electrically connected to the high-frequency power source 120 via the sample table shaft 60. Further, the buffer chamber 10 and the high-frequency power source 120 are grounded, respectively. The sample 70 can be controlled to a predetermined temperature via the sample table 61.

In Fig. 1, the discharge tube 21 is airtightly provided on the top wall 1 of the buffer chamber 10 being corresponded to the opening 13. The discharge tube 21 has nearly a cylindrical shape, one end thereof being nearly flat and closed and the other end thereof being open. A waveguide 32 is arranged on the outside of the discharge tube 21 to include the discharge tube 21 therein. The axis of the waveguide 32 is nearly in agreement with that of the discharge tube 21. A sample table shaft 62 is studied on the bottom wall 14 of the buffer chamber 10. A sample table 63 is provided nearly horizontally at the upper end of the sample table shaft 62. The sample table 63 has the shape of a plane which is smaller than the opening 13 but is greater than the sample 70. The sample table 63 has a plane for placing the sample on the front surface thereof, i.e., on the surface opposed to the closed end of the discharge tube 21. The axes of the sample table shaft 62 and the sample table 63 are nearly in agreement with the axis of the discharge tube 21. A metallic bellows 82 is provided to surround the sample table shaft 62 in the buffer chamber 10. The lower end of the bellows 82 is provided inside the bottom wall 14 of the buffer chamber 10. A flange 83 is provided at the upper end of the bellows 82. A sealing ring (not shown) is provided on the surface of the flange 83 opposed to the inner surface of top wall 11 of the buffer chamber 10. There is further provided means (not shown) for expanding and contracting the bellows 82. Space 91 is defined being airtightly shut off from the interior of the buffer chamber 10 under the condition where the bellows 82 is expanded by expansion-contraction drive means and the flange 83 is pressed via the sealing ring onto the inner surface of top wall 11 of the buffer chamber 10. An evacuation nozzle 101 is formed in the bottom wall 14 of the buffer chamber 10 to be communicated with the space 91. An evacuation pipe (not shown) coupled to an evacuation device (not shown) is coupled to the evacuation nozzle 101. The evacuation pipe is provided with a switching valve and an evacuation resistance variable valve (not shown). A gas introduction path 115 is formed in the top wall 11 of the buffer chamber 10 so as to be communicated with the space 91. A gas introduction pipe 117 coupled to a source 116 of gas for after-treatment is coupled to the gas introduction path 115. The gas introduction pipe 117 is provided with the switching valve and a gas flow rate control device (not shown). In Fig. 1, reference numeral 130 denotes a reflection end.

In Fig. 1, furthermore, provision is made of means for conveying the sample 70 into the buffer chamber 10 to hand it over onto the sample-placing surface of the sample table 61, means for conveying the sample 70 from the sample table 61 to the sample table 63 through the buffer chamber 10, and means (none of these means are shown) which receives the sample 70 from the sample table 63 and carries it out of the buffer chamber 10.

In Fig. 1, the bellows 80 and 82 are contracted by their respective expansion-contraction drive means. Under this condition, the evacuation means is operated so that the interiors of the buffer chamber 10 and the discharge tubes 20, 21 are evacuated into a predetermined pressure. Thereafter, the sample 70, one sample in this case, is conveyed into the buffer chamber 10 and is placed with its surface to be treated being faced upwards on the sample-placing surface of the sample table 61. Thereafter, the space 90 is formed. The predetermined etching gas is introduced at a predetermined rate from the source 111 of etching gas into the space 90. In this case, no anticorrosion gas is introduced from the source 113 of anticorrosion gas into the space 90. The etching gas in space 90 is partly evacuated via the evacuation nozzle 100 such that the pressure in space 90 is adjusted to predetermined value for effecting the etching. Furthermore, a microwave electric field is generated by the magnetron 40 and a magnetic field is generated by the solenoid coil 50. The etching gas in the discharge tube 20 in space 90 is plasmatized owing to the synergistic action of the microwave electric field and the magnetic field. The surface to be treated of the sample 70 placed on the sample-placing surface of the sample table 61 is etched with the plasma. During the etching, a high-frequency bias is applied to the sample 70 whose temperature is controlled to a predetermined value via the sample table 61. When the etching is finished, introducing of the etching gas is stopped, and operations of the magnetron 40, solenoid coil 50, and high-frequency power source 120 are stopped too.

Thereafter, the space 90 is evacuated again to a predetermined pressure. Further, the switching value provided for the gas conduit 114 is opened. That is, the predetermined anticorrosion gas is introduced at a predetermined flow rate from the source 113 of anticorrosion gas into the space 90 that is evacuated to a predetermined pressure instead of the etching gas. The anticorrosion gas in space 90 is partly evacuated

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through the evacuation nozzle 100 such that the pressure in space 90 is adjusted to a predetermined value for anticorrosion treatment. On the other hand, the microwave electric field is generated by the magnetron 40 and the magnetic field is generated by the solenoid coil 50. The anticorrosion gas in the discharge tube 20 in space 90 is plasmatized owing to the synergistic action of the microwave electric field and the magnetic field. The etched sample 70 placed on the sample-placing surface of the sample table 61 is anticorrosion-treated by utilizing the plasma. That is, the matter formed by the etching with plasma and adhered to the sample 70 is removed from the sample 70. During the anticorrosion treatment, a high-frequency bias is applied to the sample 70 that is etched, and the temperature of the etched sample 70 is controlled to a predetermined value via the sample table 61. At a moment when the anticorrosion treatment is finished, introduction of the anticorrosion gas is stopped, and operations of the magnetron 40, solenoid coil 50 and high-frequency power source 120 are stopped too. Thereafter, the bellows 80 is contracted.

Then, under this condition, the sample 70 that is anticorrosion-treated is conveyed from the sample table 61 to the sample table 63 through the buffer chamber 10 and is placed on the sample-placing surface of the sample table 63 with its surface to be treated being faced upwards. Then, the space 91 is formed. A predetermined gas for after-treatment such as a gas for resist ashing and a gas for passivation is introduced at a predetermined flow rate from the source 116 of after-treatment gas into the space 91. The gas for after-treatment in space 91 is partly evacuated through the evacuation nozzle 101 such that the pressure in space 91 is adjusted to a predetermined value for after-treatment. A microwave electric field is generated by the magnetron 41, and the gas for after-treatment in the discharge tube 21 in space 91 is plasmatized by the action of the microwave electric field. The sample 70 placed on the sample-placing surface of the sample table 63 is subjected to the after-treatment such as the resist ashing or the passivation utilizing the plasma. At a moment when the after-treatment is finished, introduction of the gas for after-treatment is stopped and the operation of the magnetron 41 is stopped too. Then, the bellows 82 is contracted. Under this condition, the sample 70 that is treated is removed from the sample table 63 and is taken out of the buffer chamber 10.

The aforementioned treatment operations are successively carried out, and the sample is treated one by one continuously.

The sample 70 may, for example, be the one that is shown in Fig. 2. That is, the sample 70 in Fig. 2 has a laminated-layer structure which consists of a TiN film 72 which is a barrier metal formed on a silicon oxide film 71 which is an underlying oxide film, an Al-Cu-Si alloy film 73 formed thereon, and a cap metal 72 formed further thereon. A resist 75 is formed on the cap metal 74. Here, the barrier metal is used for preventing the precipitation of silicon on the contact portions where the silicon oxide film 71 and the Al-Cu-Si alloy film 73 are electrically connected together and for preventing the wiring from being broken by the electromigration or the stress migration. In addition to the TiN film 71, the barrier metal may be a high-melting metal film of the type of, for example, TiW, TiW-Ti, TiN/Ti, MoSi<sub>2</sub>, WSi<sub>2</sub>, or W, or an alloy film thereof. Like the barrier metal, the cap metal 74 works to prevent the wiring from being broken by the electromigration or the stress migration and further works to prevent the halation when the resist film is exposed to the beam. As the cap metal 74, there is used a film composed of TiN, MoSi<sub>2</sub>, TiW, polysilicon, WSi<sub>2</sub> or the like.

In this case, the gas for etching consists of a halogen gas containing, for example, chlorine, such as a BC<sub>l</sub><sub>3</sub> + Cl<sub>2</sub> mixture gas. In Fig. 1, the BC<sub>l</sub><sub>3</sub> + Cl<sub>2</sub> mixture gas in the discharge tube in space 90 is plasmatized by the synergistic action of the microwave electric field and the magnetic field. The sample 70 shown in Fig. 2 is etched by utilizing the plasma. The conditions for etching in this case are as follows:

45	Flow rate of etching gas that is introduced	BC <sub>l</sub> <sub>3</sub> : 40 cc/min. Cl <sub>2</sub> : 60 cc/min.
50	Pressure for etching Microwave power Magnetic field intensity High-frequency bias power Temperature of sample 70	10 mTorr 700 W 875 Gausses 70 W 40 °C

Fig. 3 is a vertical section view of the sample 70 that is etched under the above-mentioned conditions. As shown in Fig. 3, matters (reaction products and chlorides of etching gas components) 140 adhere to the side walls and to the surface of the resist 75. The sample 70 thus etched is anticorrosion-treated with the

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plasma using a chlorine gas ( $\text{Cl}_2$ ) as an anticorrosion gas. That is, in Fig. 1,  $\text{Cl}_2$  in the discharge tube 20 in space 90 is plasmatized by the synergistic action of the microwave electric field and the magnetic field. The etched sample 70 shown in Fig. 3 is anticorrosion-treated by utilizing the plasma. In this case, the anticorrosion treatment conditions are as follows:

5	Flow rate of anticorrosion gas that is introduced	$\text{Cl}_2$ : 90 cc:min.
10	Pressure for anticorrosion treatment	10 mTorr
	Microwave power	700 W
15	Magnetic field intensity	875 Gausses
	High-frequency bias power	40 W
20	Discharge (anticorrosion treatment) time	20 sec.
	Temperature of sample 70	40 °C

The matters 140 containing chlorine adhered to the etched sample 70 are removed from the etched sample 70 as the matters 140 react with chlorine ions and chlorine radicals in the plasma of  $\text{Cl}_2$  gas. No new matter adheres to the etched sample 70 in the anticorrosion treatment. When the discharge (anticorrosion treatment) time is shorter than 20 seconds, the matters are not sufficiently removed from the etched sample 70. Therefore, the discharge (anticorrosion treatment) time should be about 20 seconds at the shortest. When the discharge (anticorrosion treatment) time is too long, however, the wiring film itself is etched and the wiring becomes thinner than a predetermined pattern. The thus anticorrosion-treated sample 70 is subjected to the after-treatment and is then taken out of the buffer chamber 10. In the after-treatment, in this case, the resist ashing and the passivation are effected simultaneously. That is, an oxygen gas or a gas containing oxygen is used as a gas for the after-treatment, the resist 75 is removed from the anticorrosion-treated sample 70 by utilizing the plasma of the gas for after-treatment and, at the same time, a passivation film is formed on the pattern surface. The sample 70 is then left to stand in the open air. Even when it is left to stand for 48 hours, there is observed no corrosion of the sample 70. By effecting the passivation treatment in addition to the anticorrosion treatment, the above effect is further promoted owing to the function of the passivation film that is formed on the pattern surface.

The same results are also obtained even when use is made, as an anticorrosion gas, of an inert gas such as helium, argon, or a mixture gas consisting of the chlorine gas and the inert gas. When, for example, an inert gas is used as the anticorrosion gas, only the sputtering action takes place without participating in the chemical reaction and without forming any matter that adheres. Therefore, the same results are obtained as those of when the chlorine gas is used as the anti corrosion gas. When the anticorrosion treatment is carried out under the following conditions by using an argon as as the anticorrosion gas, there are obtained the same effects as those of when the chlorine gas is obtained.

40	Flow rate of anticorrosion gas that is introduced	$\text{Ar}$ : 50 cc:min.
45	Pressure for anticorrosion treatment	6 mTorr
	Microwave power	700 W
	Magnetic field intensity	875 Gausses
	High-frequency bias power	50 W
	Discharge (anticorrosion treatment) time	60 sec.
	Temperature of sample 70	40 °C

When the discharge (anticorrosion treatment) time is shorter than 60 seconds, the adhered matters 140 are not sufficiently removed from the etched sample 70. Therefore, the discharge (anticorrosion treatment) time should be about 60 seconds at the shortest. Even when the discharge (anticorrosion treatment) time is longer than 60 seconds, the aforementioned inconvenience develops little unlike the case of when the chlorine gas is used as the anticorrosion gas.

The same results are obtained even when use is made, as the anticorrosion gas, of a mixture gas containing at least 90% of chlorine gas (the remainder being the one other than the inert gas). Examples of the remainder gas other than the inert gas to be added to the chlorine gas include those gases that do not deposit such as  $\text{SF}_6$ ,  $\text{Br}_2$  and the like. Here, for instance, the sample has a laminated-layer structure which comprises a TiW film that is a barrier metal on a silicon oxide film that is the underlying oxide film, and an

Al-Cu alloy film with a regist being formed on the Al-Cu alloy film. When the sample etched under the same etching conditions as those for the sample 70 is anticorrosion-treated using a Cl<sub>2</sub> + SF<sub>6</sub> mixture gas as the anticorrosion gas, there are obtained the same effects as those mentioned above. In this case, the flow rates for introducing the anticorrosion gases are 90 cc/min. for Cl<sub>2</sub> and 5 cc/min. for SF<sub>6</sub>, and other anticorrosion treatment conditions are the same as those of when the chlorine gas is used as the anticorrosion gas.

The aforementioned embodiments are particularly preferred when the sample includes aluminum and, particularly, an aluminum film, an aluminum alloy film (e.g., aluminum alloy film containing 0.5 to 5% of copper), or when the sample has the laminated-layer structure consisting of these films and a barrier metal.

In addition to the above-mentioned embodiments, furthermore, there may be used ozone to subject the anticorrosion-treated sample 70 to the passivation treatment. In this case, means for plasmatization used in the above embodiment is not necessary but, instead, there must be used means for generating ozone and means for introducing ozone used by the above means into the space 91. Moreover, if ozone is irradiated with ultra-violet rays (UV), the passivation film formed on the pattern surface becomes more dense and solid presenting desirable properties from the standpoint of avoiding corrosion.

The aforementioned embodiments offer the following effects.

(1) No wet-type anticorrosion treatment is necessary, making it possible to greatly reduce the time required for anticorrosion-treating the sample and to increase the throughput.

(2) The wet-type anticorrosion treatment technology requires the wet-type anticorrosion treatment apparatus and a drying apparatus. The embodiment of the invention, however, requires no drying apparatus making it possible to decrease the cost of the apparatus and to decrease the area occupied by the apparatus.

(3) There is no need of recovering the waste liquor or treating the waste liquor, and the apparatus is simply constructed at a reduced cost.

(4) The etching treatment and the anticorrosion treatment are carried out in the same chamber, and the sample needs not be conveyed from the etching treatment unit to the anticorrosion treatment unit. Therefore, the time required for anticorrosion-treating the sample is further shortened contributing to further enhancing the throughput.

(5) The etching treatment and the anticorrosion treatment are carried out in the same chamber, making it possible to decrease the cost of the apparatus and to decrease the area occupied by the apparatus.

(6) The sample can be overetched by utilizing the plasma of an anticorrosion gas. In this case, the etching gas and the anticorrosion gas can be switched by the time control or by an etching completion discrimination signal from an etching completion detect means (not shown).

(7) The sample can be anticorrosion-treated by utilizing the plasma of an anticorrosion gas while the sample is being etched utilizing the plasma of an etching gas containing the anticorrosion gas. When the sample is being etched, in this case, the etching gas and the anticorrosion gas can be introduced being switched alternately.

The above-mentioned treatment can be put into practice by using an apparatus having separate spaces (i.e., having two treating chambers) for the etching treatment and the anticorrosion treatment instead of the aforementioned embodiments.

In the above embodiments, the sample is etched with the plasma generated by the microwave electric discharge in the presence of a magnetic field and is then anticorrosion-treated utilizing the plasma generated by the microwave electric discharge in the presence of a magnetic field. However, there is no particular limitation with regard to what sort of electric discharge is used to generate the plasma. For instance, the sample after etched with plasma may be anticorrosion-treated by utilizing the plasma that is generated by the dc electric discharge, ac electric discharge (high-frequency electric discharge), or high-frequency discharge in the presence of a magnetic field such as magnetron discharge. Furthermore, the anticorrosion treatment may be effected by utilizing the plasma generated by the microwave electric discharge in the absence of magnetic field. In this case, it is desired to apply a bias to the sample that is anticorrosion-treated.

Furthermore, the anticorrosion gas may be plasmatized not based on the electric discharge but using any other form of energy such as light energy (photo-excitation).

In the aforementioned embodiments, furthermore, the etching gas and the anticorrosion gas are plasmatized in the treating chamber. It is, however, also allowable to plasmatize the etching gas and the anticorrosion gas outside the treating chamber and to convey (transit) the plasma into the treating chamber. In this case, the sample after etched with plasma is anticorrosion-treated by utilizing the plasma of anticorrosion gas that is formed outside the treating chamber and that is conveyed (transited) into the

treating chamber. Furthermore, the sample is etched with the plasma of an etching gas that is generated outside the treating chamber and is conveyed (transited) into the treating chamber, and the etched sample is anticorrosion-treated by utilizing the plasma of anticorrosion gas that is generated outside the treating chamber and is conveyed (transited) into the treating chamber.

5 According to the present invention, there can be used samples of the laminated-layer structure consisting of metal films such as of aluminum, silicon, copper, tungsten, titanium, molybdenum and the like, or alloy films thereof, or alloy films of these metals and silicon, or these films and high-melting metals such as tungsten and molybdenum, and silicide films thereof or TiN and TiW films.

10 According to the present invention as described above, the wet-type anticorrosion treatment is not required enabling the throughput to be increased in treating the samples that must be etched and anticorrosion-treated.

### Claims

- 15 1. A method of etching a sample comprising the steps of plasmatizing a halogen gas as an etching gas, etching a sample by the plasma of said etching gas, and anticorrosion-treating the etched sample by a plasma of a gas containing a halogen gas or an inert gas as an anticorrosion gas that is capable of removing from said etched sample adhered matters containing halogen formed by the etching of said sample.
- 20 2. A sample treating method according to claim 1, wherein said sample has an aluminum film, an aluminum alloy film, or films of a multi-layer structure consisting of one or more of such films and a barrier metal, which film or films are etched by said plasma of a halogen gas, and anticorrosion treated by said plasma of said anticorrosion gas.
- 25 3. A sample treating method according to claim 1 or claim 2, wherein said etching gas comprises chlorine, and said anticorrosion gas comprises chlorine.
- 30 4. A sample treating method according to claim 1 or claim 2, wherein said etching gas comprises chlorine and said anticorrosion gas is an inert gas.
- 35 5. A sample treating method according to claim 1 or claim 2, wherein said etching gas comprises chlorine, and said anti-corrosion gas is a mixture gas which consists of chlorine gas and at least one other gas other than an inert gas and having no deposition property, said chlorine gas being present in said mixture gas in an amount of at least 90%.
- 40 6. A sample treating method according to any one of claims 1 to 5, wherein said etching gas comprises a halogen gas, and the anticorrosion-treated sample is passivation-treated by a plasma of an oxygen gas or a gas that contains oxygen.
- 45 7. A sample treating method according to any one of claims 1 to 6, wherein said etching gas comprises a halogen gas, and the anticorrosion-treated sample is passivation-treated by ozone.
- 50 8. A sample treating method according to any one of claims 1 to 7, wherein said anticorrosion gas is plasmatized by the synergistic action of a microwave electric field and a magnetic field, and a bias is applied to said sample while it is being anticorrosion-treated by the plasma of said anticorrosion gas.
- 55 9. A sample treating method according to any one of claims 1 to 8, wherein the etching and the anticorrosion treatment of said sample are carried out in the same or different treating spaces.
10. An apparatus for etching a sample with a plasma of a halogen gas as an etching gas and anticorrosion-treating the etched sample, comprising means (20,30,31,40,50) for plasmatizing a gas containing a halogen gas or inert gas and an anticorrosion gas that is capable of removing adhered matters containing halogen formed by the etching of said sample, means (60,61) for holding said etched sample while it is anticorrosion-treated by the plasma of said anticorrosion gas, and a treating chamber (10,12,20,80,81) that is evacuated and contains said sample-holding means (60,61) therein.
- 55 11. A sample treating apparatus according to claim 10, wherein said means (20,30,40,50) for plasmatizing the etching gas acts by synergistic action of a microwave electric field and a magnetic field, said etching gas being introduced into the treating chamber (10,12,20,80,81) by means (110 to 112) for introducing said etching gas, and said means (20,30,40,50) for plasmatizing said anticorrosion gas also acts by the synergistic action of a microwave electric field and a magnetic field, said anticorrosion gas being introduced into the anticorrosion-treating chamber (10,12,20,80,81) by means (110,112 to 114) for introducing said anticorrosion gas, and said sample-holding means (60,61) for the sample to be anticorrosion-treated is biased.
12. A sample treating apparatus according to claim 11, wherein a high-frequency power source (120) is connected to said sample-holding means (60,61).

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13. A sample treating apparatus according to claim 11 or claim 12 wherein said etching gas and said anticorrosion gas are introduced into the same sample treating chamber.

14. A sample treating apparatus according to claim 13, wherein means (110 to 114) for introducing said etching gas and said anticorrosion gas into said treating chamber (10,12,20,80,81) includes means that 5 switches the introduction of said etching gas and said anticorrosion gas into said treating chamber.

15. A sample treating chamber according to claim 11 or claim 12, wherein said treating chamber into which said etching gas is introduced is different from said treating chamber into which said anticorrosion gas is introduced.

16. An apparatus for etching a sample by a plasma of an etching gas and anticorrosion-treating said 10 etched sample, comprising means (20,30,31,40,50) for plasmatizing an anticorrosion gas that is capable of removing adhered matters formed by the etching of said sample, a treating chamber (10,12,20,80,81) in which the etched sample is anticorrosion-treated by a plasma of said anticorrosion gas, and a treating chamber (10,13,21,82,83) in which the anticorrosion-treated sample is passivation-treated.

17. A sample treating apparatus according to claim 16, wherein the treating chamber (10,13,21,82,83) 15 for said passivation treatment is arranged to effect the passivation treatment with a plasma of an oxygen gas or a gas containing oxygen.

18. A sample treating apparatus according to claim 16, wherein the treating chamber (10,13,21,82,83) for said passivation treatment is arranged to effect the passivation treatment with ozone.

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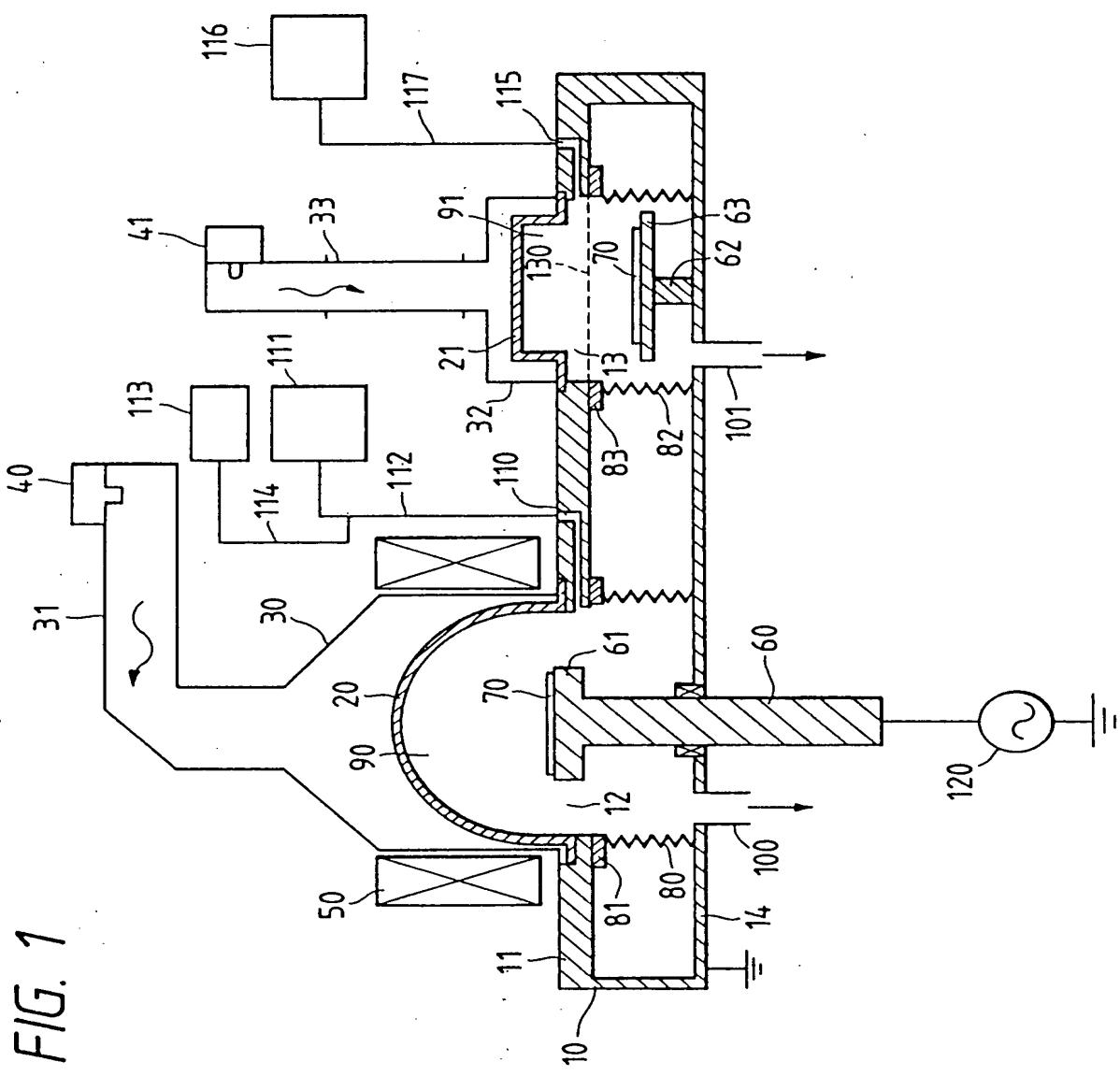


FIG. 2

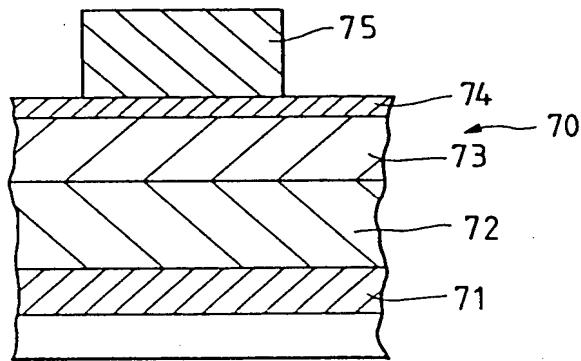
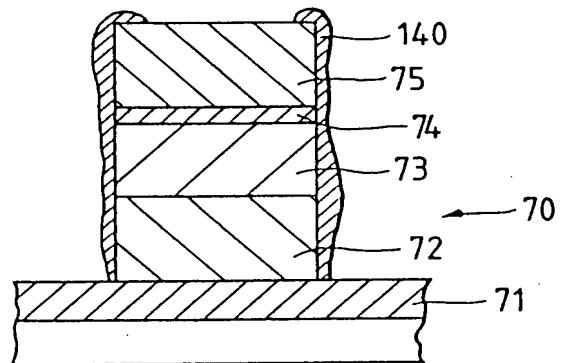


FIG. 3





European Patent  
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## EUROPEAN SEARCH REPORT

Application Number

EP 90 30 2566

DOCUMENTS CONSIDERED TO BE RELEVANT													
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int. Cl.5)										
A	GB-A-2 166 590 (OERLIKON-BUHRLE) * Claims 10,16 * ---	1-3,5,9, ,15	H 01 L 21/321										
A	PROCEEDINGS OF THE ELECTROCHEMICAL SOCIETY, vol. 83, 1983, pages 341-352; T. TSUKADA et al.: "After corrosion treatment in aluminum alloy reactive ion etching" * Whole document * -----	6,9,10, 13,14, 17 /											
TECHNICAL FIELDS SEARCHED (Int. Cl.5)													
H 01 L													
<p>The present search report has been drawn up for all claims</p> <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 33%;">Place of search</td> <td style="width: 33%;">Date of completion of the search</td> <td style="width: 34%;">Examiner</td> </tr> <tr> <td>THE HAGUE</td> <td>14-06-1990</td> <td>PHEASANT N.J.</td> </tr> </table>				Place of search	Date of completion of the search	Examiner	THE HAGUE	14-06-1990	PHEASANT N.J.				
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<p>CATEGORY OF CITED DOCUMENTS</p> <table border="0" style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 33%;">X : particularly relevant if taken alone</td> <td style="width: 33%;">T : theory or principle underlying the invention</td> </tr> <tr> <td>Y : particularly relevant if combined with another document of the same category</td> <td>E : earlier patent document, but published on, or after the filing date</td> </tr> <tr> <td>A : technological background</td> <td>D : document cited in the application</td> </tr> <tr> <td>O : non-written disclosure</td> <td>L : document cited for other reasons</td> </tr> <tr> <td>P : intermediate document</td> <td>&amp; : member of the same patent family, corresponding document</td> </tr> </table>				X : particularly relevant if taken alone	T : theory or principle underlying the invention	Y : particularly relevant if combined with another document of the same category	E : earlier patent document, but published on, or after the filing date	A : technological background	D : document cited in the application	O : non-written disclosure	L : document cited for other reasons	P : intermediate document	& : member of the same patent family, corresponding document
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